

Note

Gaussian Quadrature Formulas for the Numerical Calculation of Integrals with Logarithmic Singularity

The double integral

$$I = \int_0^1 \int_0^1 f(x, y)/(x - y) dx dy \tag{1}$$

with Cauchy-type singularity arises in the study of aerodynamic or hydrodynamic load on a lifting body [1, 2]. Applying an ingenious substitution, Song [3] has transformed (1) into

$$I = I_1 + I_2 \tag{2}$$

where

$$I_1 = \int_0^1 \int_0^1 [f(yt, y) - f(yt - t + 1, y)]/(t - 1) dt dy \tag{3}$$

and

$$I_2 = \int_0^1 \ln[(1 - y)/y] f(y, y) dy. \tag{4}$$

If f and $\partial f/\partial x$ are bounded for $-1 \leq x, y \leq 1$, the double integral (3) is a proper integral which can be computed using standard cubature rules [4]. The integral (4) has two logarithmic end point-singularities. Using the substitution $x = 1 - 2y$, it can be transformed into

$$I_2 = \int_{-1}^1 \phi(x) \ln [(1 + x)/(1 - x)] dx \tag{5}$$

where

$$\phi(x) = f[(1 - x)/2, (1 + x)/2].$$

It is the purpose of this note to present a table of abscissas and weights of gaussian quadrature formulas for the evaluation of (5).

The weight function

$$w(x) = \ln[(1 - x)/(1 + x)] \tag{6}$$

in (5) is an odd function and consequently [5], the $2N$ -point gaussian quadrature formula

$$\int_{-1}^1 \phi(x) \ln[(1+x)/(1-x)] dx \simeq \sum_{k=1}^N w_k [\phi(x_k) - \phi(-x_k)], \quad N = 1, 2, \dots \quad (7)$$

exists. The abscissas x_k and weights w_k are given by $x_k = u_k^{1/2}$ and $w_k = v_k/x_k$, $k = 1, 2, \dots, N$, where u_k and v_k are the abscissas and weights of the Gaussian N -point formula

$$\int_0^1 \ln[(1+u^{1/2})/(1-u^{1/2})] \psi(u) du \simeq 2 \sum_{k=1}^N v_k \psi(u_k). \quad (8)$$

Since the weight function in (8) is nonnegative and since all moments

$$m_i = \int_0^1 \ln[(1+u^{1/2})/(1-u^{1/2})] u^i du = 2(i+1)^{-1} \sum_{j=1}^{i+1} (2j-1)^{-1}, \quad (9)$$

$i = 0, 1, 2, \dots$ exist, the quadrature formula (8) has real abscissas u_k in the interval $(0, 1)$, and has positive weights v_k . Several algorithms for the computation of u_k and v_k using the moments (9) are described in the literature [6, 7]. However, it is well known that the construction of gaussian formulas, using ordinary moments, is strongly ill-conditioned [8]. In order to have a well-conditioned problem, we need the modified moments

$$M_i = \int_0^1 \ln[(1+u^{1/2})/(1-u^{1/2})] T_i(2u-1) du \quad (10)$$

where T_i is the Chebyshev polynomial of the first kind and of degree i . Substituting $u = x^2$ into (10) and using well-known properties of the Chebyshev polynomials [9], we obtain

$$M_i = \int_{-1}^1 \ln[(1+x)/2] [T_{2i+1}(x) + T_{2i-1}(x)] dx. \quad (11)$$

A recurrence relation for the computation of (11) is given in [10]. Now, the algorithm presented by Gautschi [8] can be applied for the construction of the Gaussian quadrature rule (8).

The abscissas and weights of the Gaussian quadrature formula (7), for $N = 2, 4, \dots, 18$ are presented in Table I. Tables for $N = 20, 30, 40$ and 50 are given in [11].

All computations are carried out on a IBM 370/158 computer, using extended precision.

TABLE I

Abscissas x_k and Weights w_k of the Gaussian Quadrature Formula

$$\int_{-1}^1 f(x) \ln[(1+x)/(1-x)] dx \simeq \sum_{k=1}^{M/2} w_k [f(x_k) - f(-x_k)]$$

M	x_k					w_k				
2	0.81649	65809	27726	03273	$E + 0$	0.12247	44871	39158	90491	$E + 1$
4	0.56318	76691	22512	76872	$E + 0$	0.62695	54799	54730	78728	$E + 0$
	0.92597	12867	85678	72798	$E + 0$	0.69862	46915	34780	84383	$E + 0$
6	0.42041	10764	80722	72115	$E + 0$	0.35227	03074	39083	73384	$E + 0$
	0.76119	37707	26794	21975	$E + 0$	0.55528	47905	05106	01731	$E + 0$
	0.96001	51738	62141	50383	$E + 0$	0.44709	95344	77937	84775	$E + 0$
8	0.33365	35398	87395	67960	$E + 0$	0.22233	21078	25118	63411	$E + 0$
	0.62837	67488	06064	89938	$E + 0$	0.38899	24551	36776	39778	$E + 0$
	0.85021	29500	95481	22025	$E + 0$	0.44310	14540	61239	04719	$E + 0$
	0.97492	63218	33825	69659	$E + 0$	0.31248	89436	79900	60742	$E + 0$
10	0.27606	36999	94800	19237	$E + 0$	0.15231	38114	13026	26769	$E + 0$
	0.53034	78820	33572	38501	$E + 0$	0.27937	41795	62341	57830	$E + 0$
	0.74291	51506	66348	11680	$E + 0$	0.35575	14413	58796	91893	$E + 0$
	0.89741	55601	15883	72284	$E + 0$	0.35373	74928	24015	70174	$E + 0$
	0.98278	34489	96595	67665	$E + 0$	0.23203	84165	55131	98034	$E + 0$
12	0.23523	12061	37427	81565	$E + 0$	0.11062	28658	52286	28071	$E + 0$
	0.45709	12029	94083	98090	$E + 0$	0.20819	16986	83831	99093	$E + 0$
	0.65301	34212	62185	31228	$E + 0$	0.27962	08746	09215	00553	$E + 0$
	0.81200	56852	61707	39870	$E + 0$	0.31132	15150	28267	40435	$E + 0$
	0.92536	73925	59699	90766	$E + 0$	0.28719	27414	80154	08687	$E + 0$
	0.98743	44128	00853	89022	$E + 0$	0.17992	65156	78923	86866	$E + 0$

Table continued

TABLE I (continued)

M	x_k					w_k				
14	0.20483	28534	68534	75454	$E + 0$	0.83892	13645	14291	27332	$E - 1$
	0.40088	24292	57998	36851	$E + 0$	0.16037	48165	78229	39720	$E + 0$
	0.57976	07843	62754	14763	$E + 0$	0.22203	29007	65799	60517	$E + 0$
	0.73385	68624	21490	26304	$E + 0$	0.26130	99860	27607	25323	$E + 0$
	0.85669	39320	52939	55269	$E + 0$	0.26998	80777	65830	49807	$E + 0$
	0.94326	51189	36524	17682	$E + 0$	0.23748	76092	42455	35127	$E + 0$
	0.99041	73891	29697	57843	$E + 0$	0.14410	45651	23003	04415	$E + 0$
16	0.18134	74152	23869	45608	$E + 0$	0.65763	00894	67130	27291	$E - 1$
	0.35662	16317	04242	97338	$E + 0$	0.12701	41957	87818	31877	$E + 0$
	0.51996	16184	25741	00152	$E + 0$	0.17924	12113	73286	79103	$E + 0$
	0.66592	46807	99086	80275	$E + 0$	0.21788	50063	52746	30233	$E + 0$
	0.78968	15473	91943	75103	$E + 0$	0.23817	11296	28565	16212	$E + 0$
	0.88719	80115	99990	89296	$E + 0$	0.23463	14570	95793	57589	$E + 0$
	0.95540	96880	96725	95703	$E + 0$	0.19969	95165	72563	29585	$E + 0$
0.99244	62781	23931	67033	$E + 0$	0.11833	96289	83263	84369	$E + 0$	
18	0.16266	90768	36973	61482	$E + 0$	0.52916	46969	11446	00491	$E - 1$
	0.32096	65862	75514	34488	$E + 0$	0.10293	09352	84617	91751	$E + 0$
	0.47064	29342	57102	99348	$E + 0$	0.14714	18102	05732	21141	$E + 0$
	0.60768	96353	12153	51892	$E + 0$	0.18263	01095	91573	47410	$E + 0$
	0.72845	30641	24958	38223	$E + 0$	0.20639	57464	14112	21728	$E + 0$
	0.82974	10530	32083	54617	$E + 0$	0.21519	10357	55009	94695	$E + 0$
	0.90892	25613	50708	79073	$E + 0$	0.20510	35892	82450	35527	$E + 0$
	0.96402	72358	73794	05301	$E + 0$	0.17039	31796	97139	97576	$E + 0$
	0.99388	96036	39699	92810	$E + 0$	0.99137	43054	21713	03975	$E - 1$

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